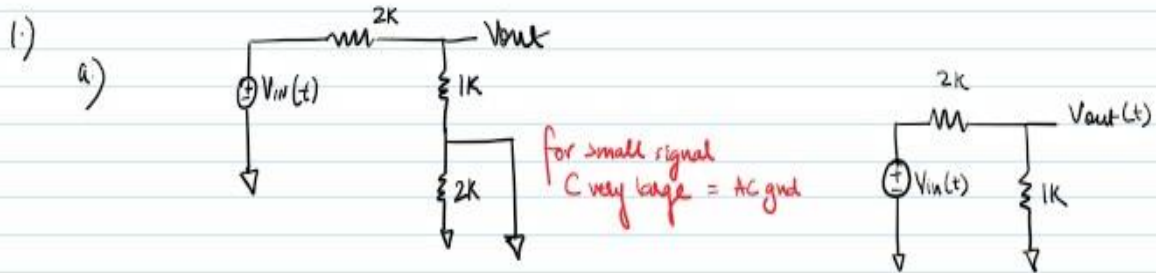
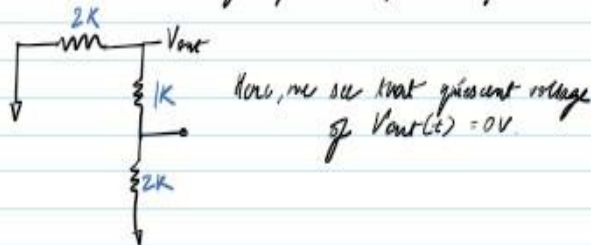


SPRING 2024

EE330 – Homework 9



b) For $V_{in}(t) = 0$ we get quiescent output voltage



c) For small signal voltage gain

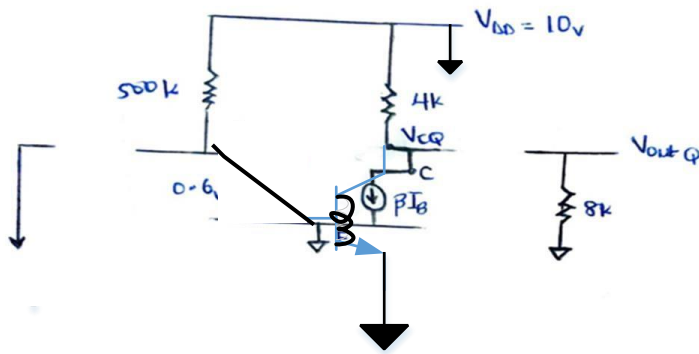
$$A_v = \frac{1K}{(1+2)K} = \frac{1}{3}$$

d) $V_{out} = A_v V_{in}(t)$

$$V_{out} = \frac{2}{3} \sin 500t$$

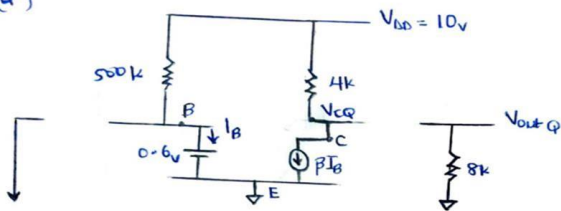
Problem 2

(a)



Problem 2

(a)



(b) - Assuming forward Active Region

$$\beta = 100$$

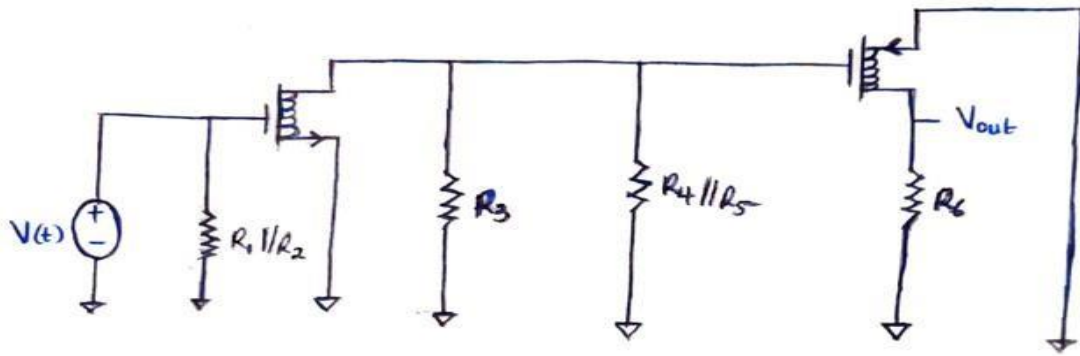
$$\rightarrow I_B = \frac{10 - 0.6}{500000} = 1.88 \times 10^{-5} A$$

$$\rightarrow I_C = \beta I_B = 100 \times 1.88 \times 10^{-5} = 1.88 \times 10^{-3} A$$

$$\rightarrow V_{CQ} = V_{DD} - (I_C \times 4k) = 10 - (1.88 \times 10^{-3} \times 4000) = 2.48V$$

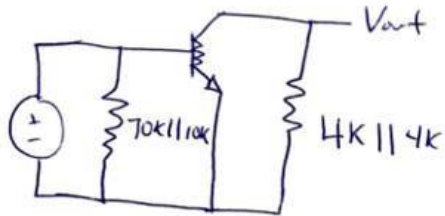
$$\rightarrow \text{since } I_{RL} = 0, V_{outQ} = I_{RL} \cdot 8k = 0$$

Problem 3



Problem 4

- (a) Draw the small signal equivalent circuit



- (b) determine V_C and V_{out}

$$V_{out} = 0V$$

$$I_C = \frac{32V - V_C}{4k\Omega}$$

$$I_C = \beta I_B$$

$$I_B + \frac{3.859}{10k} = \frac{32 - 3.859}{70k}$$

$$I_B = 16.114\mu A$$

$$\frac{32 - V_B}{70k\Omega} - \frac{V_B}{10k} + \beta \left(\frac{32 - V_B}{70k\Omega} - \frac{V_B}{10k} \right) = \frac{V_B - 0.6V}{2k}$$

$$V_B = 3.859V$$

$$\Rightarrow I_C = 100(16.114\mu A) = 1.611mA$$

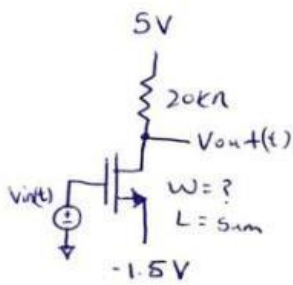
$$I_C = 1.611mA = \frac{32V - V_C}{4k\Omega}$$

$$V_C = 25.55V$$

Alternately, if we assume I_B is negligible compared to the current through the 70K resistor, the voltage at the base is, by voltage divider, $((1/8)*32V=4V$. Thus the emitter voltage is $4V-0.6V=3.4V$. So the current in the emitter, $I_E=3.4V/2K=1.7mA$. But since β is large, $I_C=I_E$. Thus $V_C=32V-I_C*4K=25.6V$.

Note this solution is somewhat simpler and the results are about the same as that obtained by including the base current.

Problem 5



(a) determine the width so that $I_D = 0.1 \text{ mA}$

$k_{COX} = 100 \mu\text{A}/\text{V}^2$ Assume Saturation

$V_{tn} = 0.75 \text{ V}$

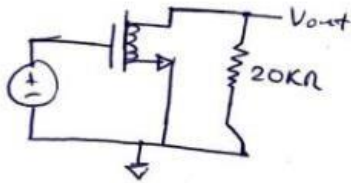
$$I_D = \frac{k_{COX}}{2} \left(\frac{W}{L}\right) (V_{GS} - V_{tn})^2$$

$$0.1 \text{ mA} = \frac{100 \mu\text{A}/\text{V}^2}{2} \left(\frac{W}{5 \mu\text{m}}\right) (1.5 - 0.75)^2$$

$$0.1 \text{ mA} = 50 \mu\text{A}/\text{V}^2 \left(\frac{W}{5 \mu\text{m}}\right) (0.75 \text{ V})^2$$

$$W = \frac{0.1 \text{ mA} \cdot 5 \mu\text{m}}{50 \mu\text{A}/\text{V}^2 \cdot (0.75 \text{ V})^2} = \underline{17.78 \mu\text{m}}$$

(b) Small signal equivalent circuit



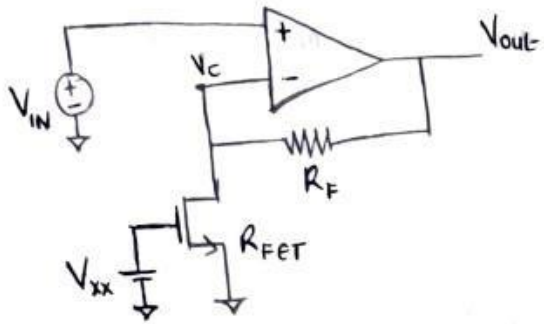
(c) determine small signal voltage gain

$$A_V = \frac{2 I_D Q R}{[V_{GS} + V_T]} = \frac{2 (0.1 \text{ mA}) (20 \text{ k}\Omega)}{[-1.5 \text{ V} + 0.75 \text{ V}]} = -5.33$$

(d) Determine THD

$$\text{THD} = \frac{V_m}{4(V_{GS} - V_T)} = \frac{200 \text{ mV}}{4(1.5 \text{ V} - 0.75 \text{ V})} = 0.067 \approx 6.7\%$$

Problem 6



* Assuming the amplifier is ideal

$$V_{in} = V_c \quad \text{--- (1)}$$

* $V_c = V_{ds}$ of the mosfet

$$V_{gs} \text{ of mosfet} = V_g - V_s = 2.5 - 0 = 2.5 \text{ v}$$

* for the mosfet to be in saturation,

$$V_{ds} \geq V_{gs} - V_{Tn}$$

Since $V_{ds} = V_c = V_{in}$, thus $V_{ds} < 10 \text{ mV}$

$\therefore V_{ds} \leq V_{gs} - V_{Tn}$ } The transistor is in triode region

(a) If $V_{XX} = 2.5 \text{ v}$, the transistor can be represented as a resistor by the channel resistance

$$R_{ch} = \frac{1}{\mu C_{ox} \frac{W}{L} (V_{gs} - V_T)} = \frac{1}{100 \times 10^{-6} \times \frac{12}{1} \times (2.5 - 0.75)}$$

$$R_{ch} = 476.19 \Omega$$

$$\text{Voltage Gain} = 1 + \frac{R_F}{476.19 \Omega}$$

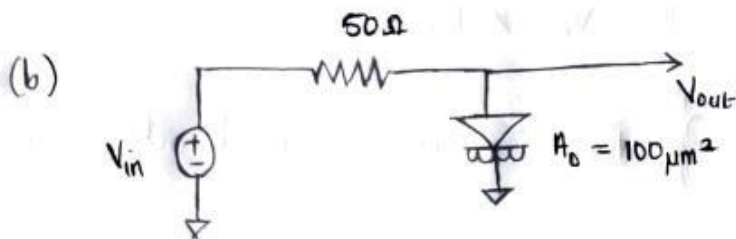
(b) From the R_{ch} equation, we notice that as V_{gs} increases, R_{ch} decreases; therefore, the gain of the noninverting amplifier increases

Problem 7

(a) No DC current goes through the capacitor

$$\rightarrow I_D = I_B = J_S A (e^{\frac{V_D}{V_T}} - 1)$$

$$\rightarrow V_D = V_T \ln \left(\frac{I_B}{J_S A} + 1 \right) = 0.026 \ln \left(\frac{1 \times 10^{-3}}{10^{-14} \times 100} + 1 \right) = 0.539 \text{ V}$$



$$(c) \quad \frac{(V_{out} - V_{in})}{50} + \frac{V_{out}}{R_D} = 0$$

$$\rightarrow V_{out} \left(\frac{1}{50} + \frac{1}{R_D} \right) = \frac{V_{in}}{50}$$

$$\rightarrow \frac{V_{out}}{V_{in}} = \frac{1}{50 \left(\frac{1}{50} + \frac{1}{R_D} \right)} = \frac{1}{1 + \frac{50}{R_D}}$$

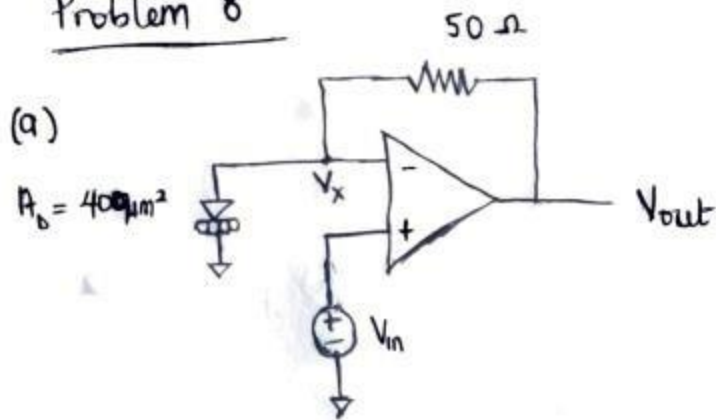
$$\text{But } R_o = \frac{V_T}{I_{\text{diode}}} = \frac{0.026}{0.001} = 26 \Omega$$

$$\Rightarrow \frac{V_{\text{out}}}{V_{\text{in}}} = \frac{1}{1 + \frac{50}{26}} = 0.342$$

$$(d) R_o = \frac{0.026}{0.005} = 5.2 \Omega$$

$$\frac{V_{\text{out}}}{V_{\text{in}}} = \frac{1}{1 + \frac{50}{5.2}} = 0.0942$$

Problem 8



(b) From the small signal equivalent circuit,

$$\frac{(V_x - V_{out})}{50} + \frac{V_x}{R_D} = 0$$

Assuming the amplifier is ideal, $V_x = V_{in}$

$$\rightarrow V_{in} \left(\frac{1}{50} + \frac{1}{R_D} \right) = \frac{V_{out}}{50}$$

$$\rightarrow \frac{V_{out}}{V_{in}} = 1 + \frac{50}{R_D}$$

$$R_D = \frac{V_T}{I_{mA}} = \frac{0.026}{0.001} = 26 \Omega$$

$$\rightarrow \frac{V_{out}}{V_{in}} = 1 + \frac{50}{26} = 2.923$$

$$(c) \frac{V_{out}}{V_{in}} = 1 + \frac{50}{R_D}$$

$$R_D = \frac{0.026}{10 \times 10^{-3}} = 2.6$$

$$\Rightarrow \frac{V_{out}}{V_{in}} = 1 + \frac{50}{2.6} = 20.23$$